

Further remarks on the pseudomomentum balance in hydro- and gasodynamics

Dalsze uwagi o bilansie pseudopędu w mechanice płynów

Janusz Badur *, Jordan Badur**

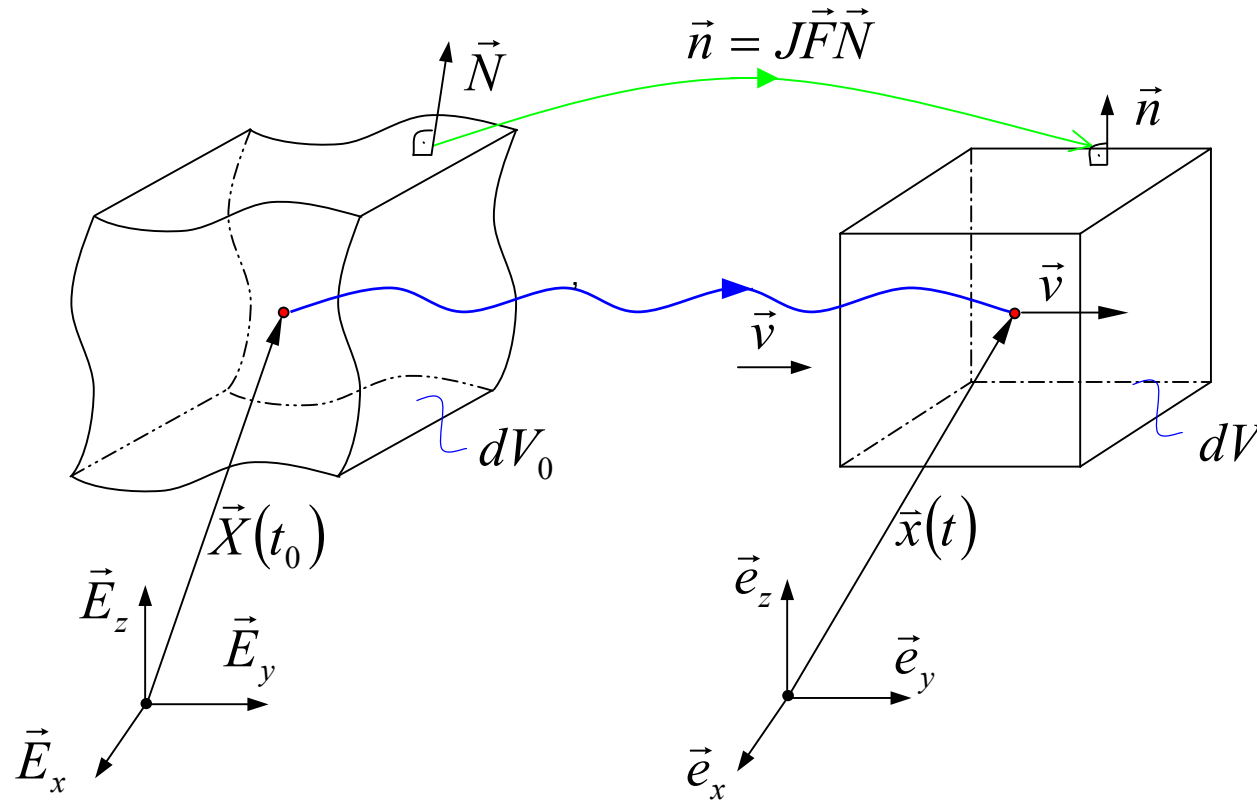
* IMP PAN Gdańsk, ** Instytut Oceanografii UG, Gdynia

Priorytety: *zrównoważone technologie energetyczne, jakość życia*

(JB) Modelowanie procesów proekologicznego spalania w urządzeniach energetycznych - fin. statutowe IMP PAN

(JB) Deterministyczne prognozy pogody Adriatyku - A. Cavalleri (Wenecja) środki grantu IP.

deformation gradient $f_{Ai} = \frac{\partial X_A}{\partial x_i}$ $F_{iA} = (f_{Ai})^{-1}$



momentum

$$p_i = \rho v_i$$

$$i = x, y, z$$

specific momentum

$$v_i$$

pseudomomentum

$$P_A = \rho_0 v_i F_{iA} = \rho_0 u_A$$

$$A = X, Y, Z$$

specific pseudomomentum

$$u_A = v_i F_{iA}$$

momentum flux

$$p_{ij} = -T_{ij} = p\delta_{ij} - (\tau_{ij} + R_{ij} + \tau_{ij}^T + \tau_{ij}^{dyf} + \tau_{ij}^{rad} + \dots)$$

pseudomomentum flux

$$P_{AB} = \rho_0(\varepsilon + \Omega - T - \theta\eta)\delta_{AB} - F_{iA}T_{iB} \quad - \text{solid}$$

$$P_{AB} = \rho_0\left(\varepsilon + \frac{p}{\rho} + \Omega - T - \theta\eta\right)\delta_{AB} = \rho_0\mu\delta_{AB} \quad - \text{fluid}$$

newtonian force density

$$b_x = b_y = 0, \quad b_z = -g,$$

configurational (pseudo) force

$$F_A^{inh} = \left(\frac{\partial L}{\partial X_A} \right)_{expl}$$

momentum balance

$$\frac{\partial}{\partial t}(\rho v_i) + \frac{\partial}{\partial x_j}(\rho v_i v_j + p_{ij}) = \rho b_i$$

pseudomomentum balance

$$\frac{\partial}{\partial t}(\rho_0 u_A) + \frac{\partial}{\partial X_B}(P_{AB}) = F_A^{inh}$$

Euler- Lagrange equation

$$E_i(L) = \frac{\partial L}{\partial x_i} - \frac{\partial}{\partial X_A} \left(\frac{\partial L}{\partial F_{iA}} \right) = 0$$

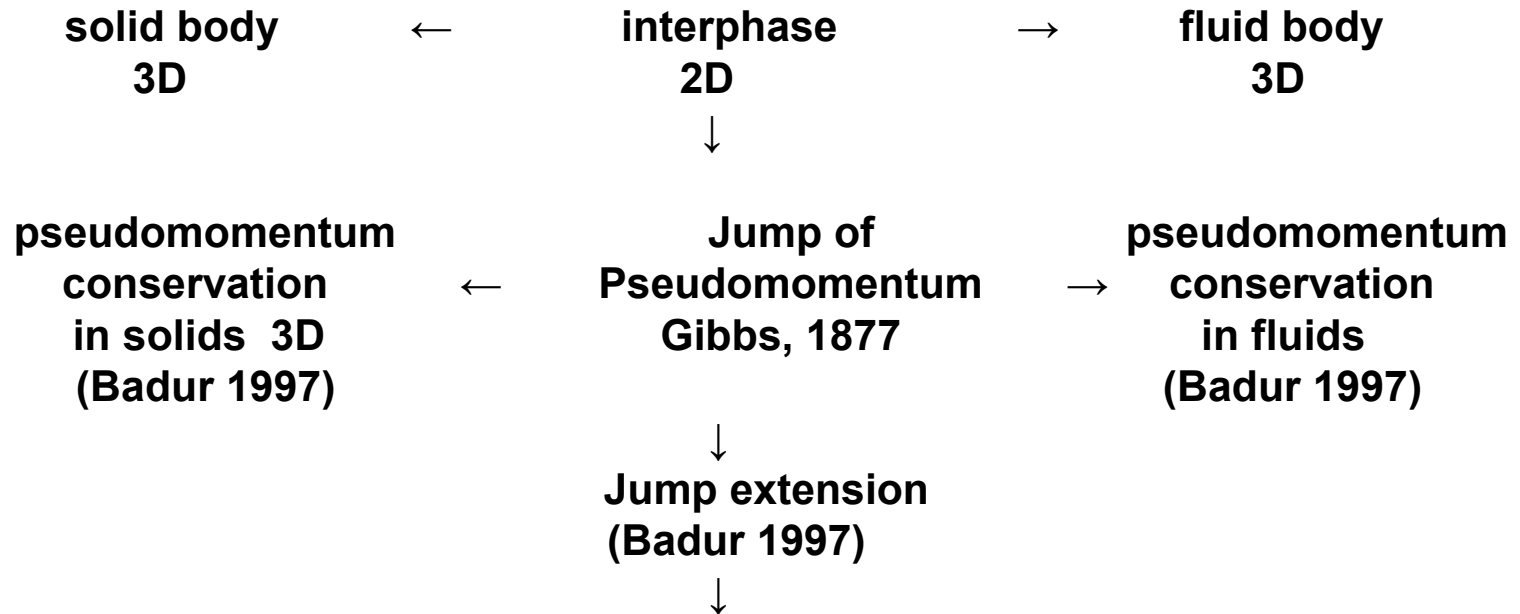
Transversality conditions

$$\frac{\partial}{\partial t}(\rho_0 u_A) + \frac{\partial}{\partial X_B}(P_{AB}) = F_A^{inh} + E_i F_{iA}$$

Pseudomomentum via Variational Principles of Thermomechanics

- Thomson – Tait , 1867
- Gibbs, 1877 (II part)
- Natanson, 1899
- Eckart , 1960

Extension of Gibbs' procedure



$$\delta_{iv} \left[\vec{\sigma} - \vec{b} \vec{C} + \vec{N} \otimes (\vec{I} - \vec{N} \otimes \vec{N}) \delta_{iv} (\vec{C} - \vec{b} \vec{K}) \right] = (\vec{P}' - \vec{P}'') \vec{N}$$

The Eckart variational principle

pseudoenergy conservation:

$$\frac{\partial}{\partial \tau} \rho_0 (T + \Omega + \varepsilon + \theta \eta) + \frac{\partial}{\partial X_A} (-p V_A) = 0$$

pseudomomentum conservation :

$$\frac{\partial}{\partial \tau} \rho_0 u_A + \frac{\partial}{\partial X_A} \rho_0 \left(\varepsilon + \frac{p}{\rho} + \Omega - \theta \eta - T \right) = 0$$

pseudo-vorticity conservation

$$w_i = \epsilon_{ijk} w_{jk} \quad w_{ij} = \frac{1}{2}(v_{j,k} - v_{k,j})$$

$$W_A = \epsilon_{ABC} W_{BC} \quad W_{BC} = \frac{1}{2}(u_{B,C} - u_{C,B})$$

$$\vec{\alpha} = \text{rot } \vec{a} = \vec{w}^t = \dot{\vec{v}} + \{tr \vec{d} \vec{I} - \vec{l}\} \vec{v}$$

Cauchy

(1815)

$$W_A = J f_{Ai} w_i \quad \text{rotor of velocity}$$

$$A_A = J f_{Ai} \alpha_i \quad \text{rotor of acceleration}$$

circulation

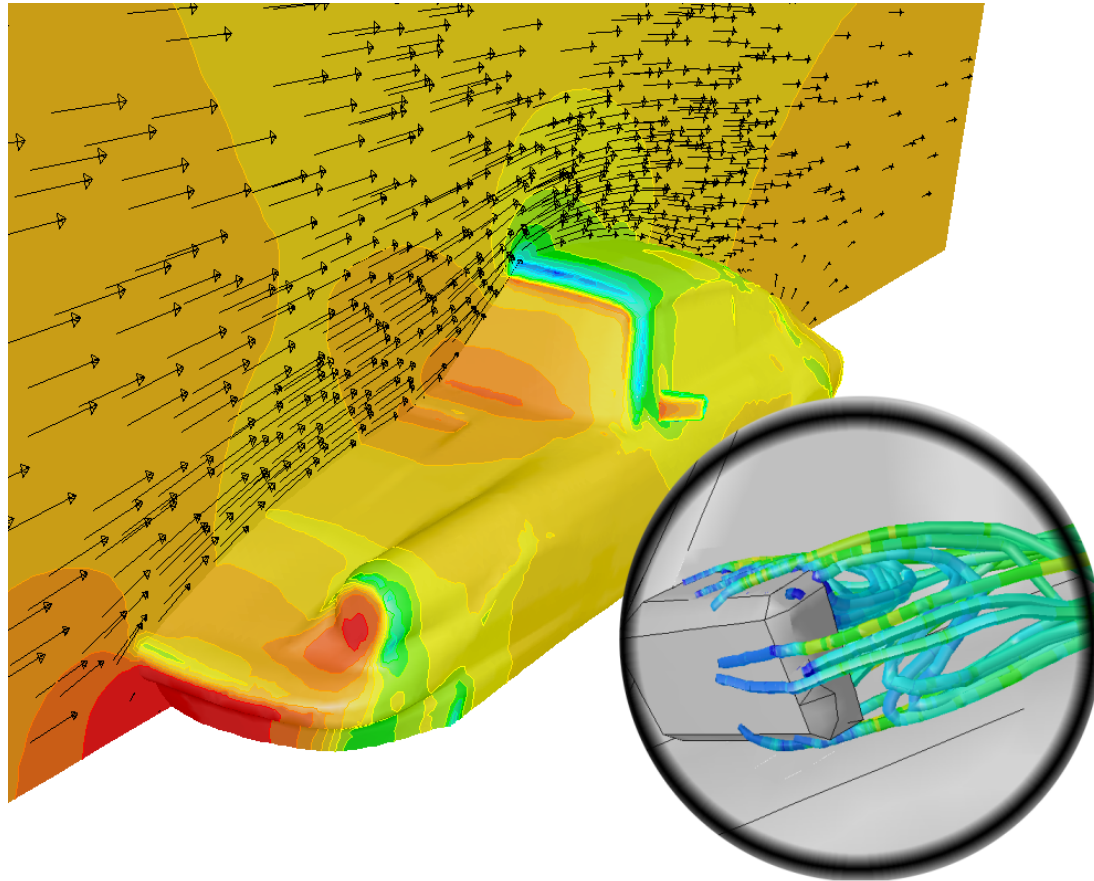
$$\Gamma = \oint_C v_i dx_i = \oiint_s w_i n_i da = \int_{C_0} u_A dX_A = \oiint_{s_0} W_A N_A dA$$

Eulerian representation of pseudomomentum

Author	Pseudomomentum flux tensor		Pseudomomentum vector	
	Lagrangean	Eulerian	Lagrangean	Eulerian
Eckart, 1960	$\alpha_{\alpha\alpha}$	—	$u_\alpha, u_\beta, u_\gamma$ *	—
Eshelby, 1970	P_{ij}	Σ_{ij}	g_i	—
Rogula, 1977	$\overline{p}_{AB}$	p_{Ai}	$\overline{p}_A$	p_A
Andrews & McIntyre, 1978	B_{ij}	—	A_i *	—
Gołębiewska–Herman, 1981	b_{ij}	B_{ik}	b_i	B_i
Grinfeld, 1981	μ_{IJ}	χ_{ij} **	—	—
Peirles, 1988	—	—	K_i ***	—
Duan, 1987	$B_{\mu\nu}$	b_{iv}	B_ν	b_ν
Maguin & Trimarco, 1992	b_{kl}	B_{ki}	P_k	jP_k
Gurtin, 1995	C_{AB}	—	—	—
present paper	P_{AB}	p_{Ai}	P_A	p_A

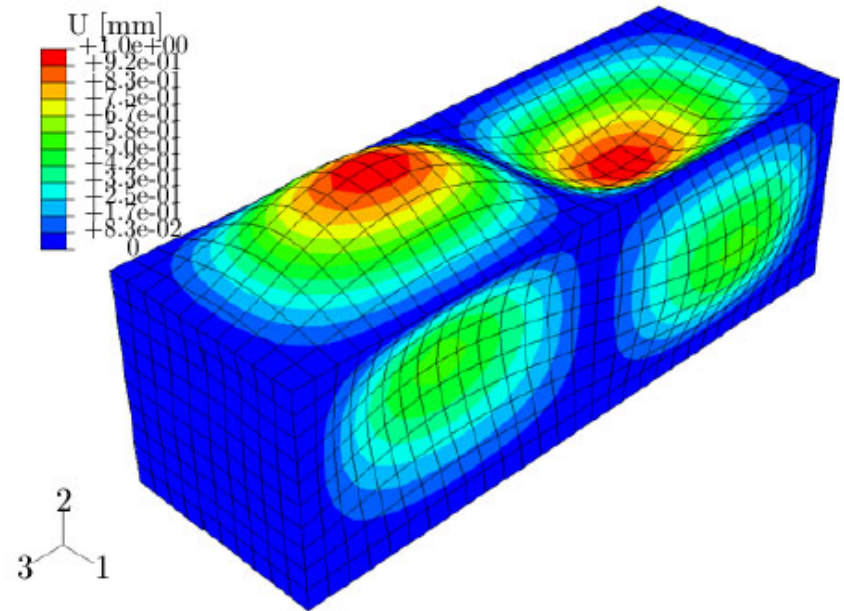
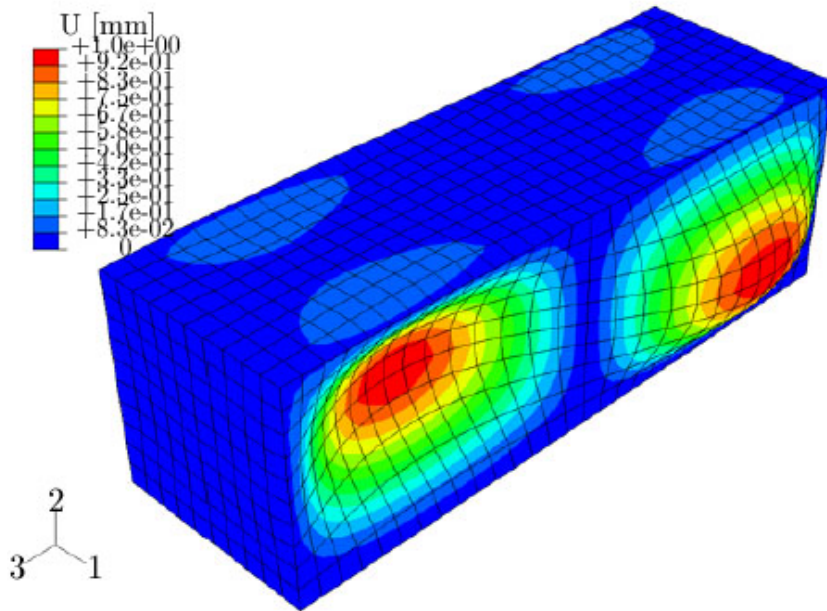
*) per unit mass **)symmetric — an analogue of the IInd Piola-Kirchhoff flux ***) in the whole volume

The acoustic pseudomomentum



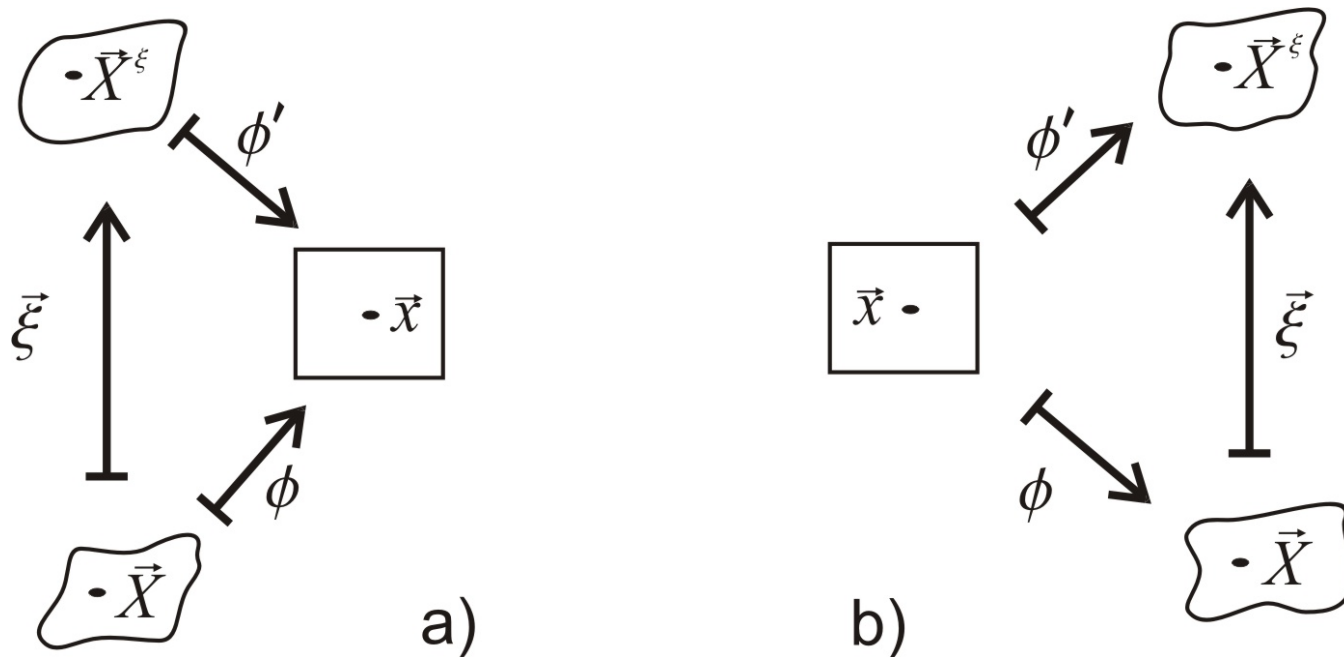
from: M. Karcz, R. Kucharski, J. Badur, Matematyczne modelowanie dźwięków generowanych przepływem czynnika roboczego, pp 1-162, submitted to: *Zesz. Nauk. IMP*, 2004

The acoustic pseudomomentum



from: R. Kucharski, A. Wiśniewski, J. Badur, Eigencharacteristics
of prestressed fluid filled tanks via an extended
Eckart coupled approach, 2004, pp 1-20, submitted to *Journal of Sound and Vibration*.

Generalized Lagrangian Mean approach



Two possible approaches for comparison of the excited motion superimposed on a normal motion of fluid element.

Andrews-McIntyre GLM (1978)

Wave displacement

$$[\xi(\vec{x}, t)]'' = 0$$

the mean Lagrangean velocity $\vec{v}^L$

the pseudomaterial derivative

$$\frac{D^L}{Dt}(\bullet) \equiv \frac{\partial}{\partial t}(\bullet) + [(\bullet) \otimes \nabla] \vec{v}^L$$

pseudomomentum balance:

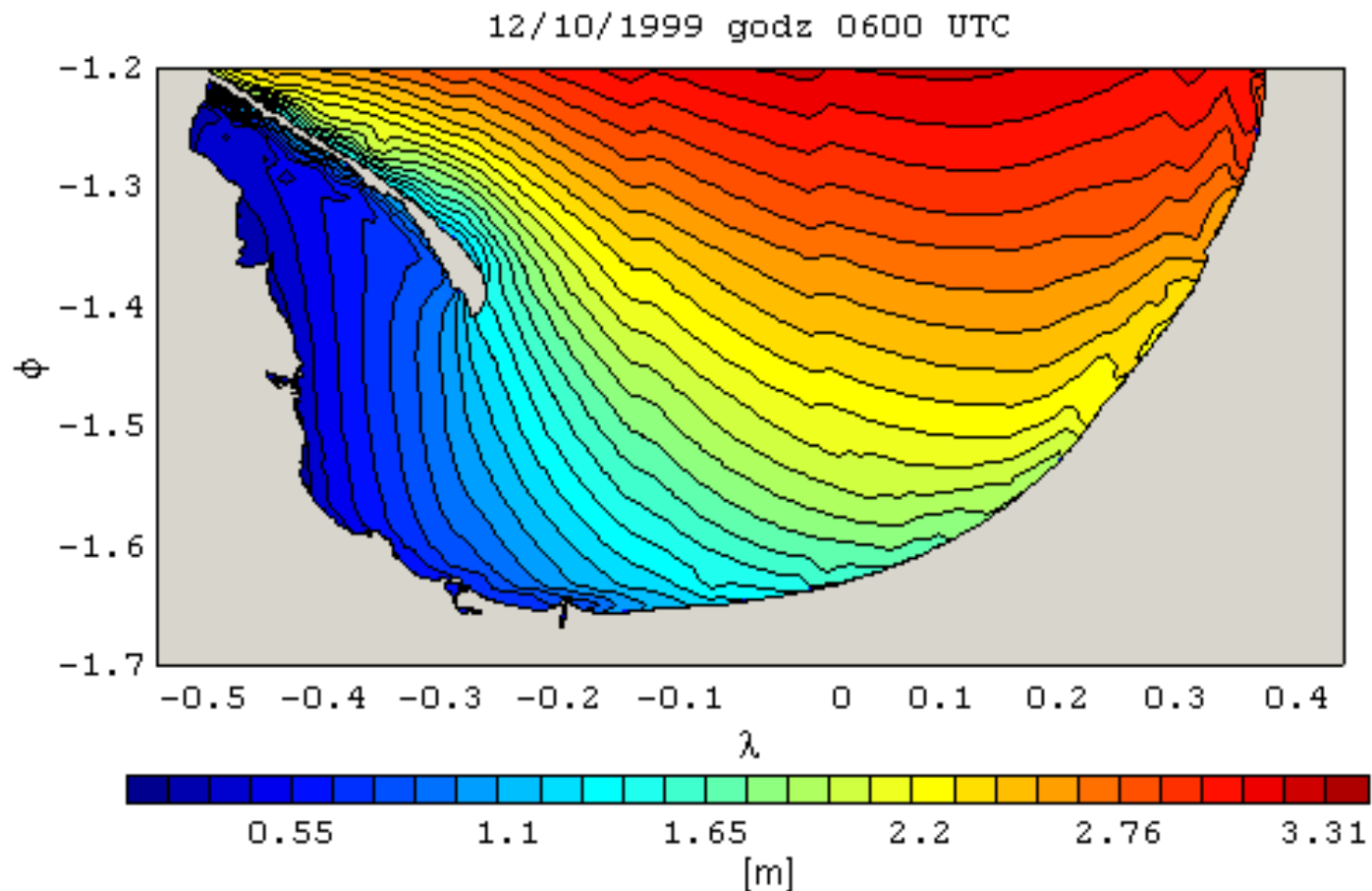
$$\frac{D^L}{Dt}(\vec{v}^L - \vec{u}^L) + (\vec{v}^L - \vec{u}^L)(\vec{v}^L \otimes \nabla) = -\nabla \pi + \vec{F}^L$$

where pseudomomentum (per unit mass)

$$\vec{u}^L = -[\xi_{j,i} \xi_{j,t}]'' \vec{e}_j$$

and

$$\pi = p^L / \rho^\xi + 1/2[\xi_{i,t} \xi_{i,t}]''$$



An example of wave action equation application in the SWAN model in the area of the Gulf of Gdańsk – Significant Wave Height H_s [m] field on the 12.10.1999

Badur J., Cieślíkiewicz W. „Parametryczny model wysokości fali znacznej i średniego okresu fali na obszarze Zatoki Gdańskiej”, Dokumentacja projektu KBN 6 P 04E 037 20

summary points

- reconstruction and revalorization of
Thompson –Tait
Gibbs → extension of Laplace formulae
Natanson
Eckart
- role of pseudomomentum in acoustics
- role of pseudomomentum in turbulence